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Large-scale instabilities of helical flows

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Large-scale hydrodynamic instabilities of periodic helical flows of a given wave number K are investigated using three-dimensional Floquet numerical computations. In the Floquet formalism the unstable field is expanded in modes of different spacial periodicity. This allows us (i) to clearly distinguish large from small scale instabilities and (ii) to study modes of wave number q of arbitrarily large-scale separation $q \ll K$. Different flows are examined including flows that exhibit small-scale turbulence. The growth rate σ of the most unstable mode is measured as a function of the scale separation $q/K \ll 1$ and the Reynolds number Re. It is shown that the growth rate follows the scaling $\sigma \propto q$ if an AKA effect [Frisch et al., Physica D: Nonlinear Phenomena 28, 382 (1987)] is present or a negative eddy viscosity scaling $\sigma \propto q^2$ in its absence. This holds both for the Re $\ll 1$ regime where previously derived asymptotic results are verified but also for Re = O(1) that is beyond their range of validity. Furthermore, for values of Re above a critical value Re_s^c beyond which small-scale instabilities are present, the growth rate becomes independent of q and the energy of the perturbation at large scales decreases with scale separation. The nonlinear behavior of these large-scale instabilities is also examined in the nonlinear regime where the largest scales of the system are found to be the most dominant energetically. These results are interpreted by low-order models.

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I. INTRODUCTION

Hydrodynamic instabilities are responsible for the frequent encounter of turbulence in nature. Although instabilities are connected to the onset of turbulence and the generation of small scales, in many situation, instabilities are also responsible for the formation of large-scale structures. In such situations, flows of a given coherence length scale are unstable to larger scale perturbations transferring energy to these scales. A classical example of a large-scale instability is the α -effect [1,2] in magneto-hydrodynamic (MHD) flows to which the origin of large-scale planetary and solar magnetic field is attributed. In α -dynamo theory, small-scale helical flows self-organize to generate magnetic fields at the largest scale of the system.

While large-scale instabilities have been extensively studied for the dynamo problem, limited attention has been drawn to large-scale instabilities of the pure hydrodynamic case. Hence, most direct numeric simulations (DNSs) and turbulence experiments are designed so that the energy injection scale ℓ is close to the domain size L. This allows us to focus on the forward energy cascade and the formation of the Kolmogorov spectrum [3]. Scales larger that the forcing scale, where no energy cascade is present, are expected [4,5] to reach a thermal equilibrium with a k^2 spectrum [6–9]. Recent studies, using (hyperviscous) simulations of turbulent flows randomly forced at intermediate scales [10], have shown that the energy spectrum at large scales deviates from the thermal equilibrium

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FIG. 1. Sketch of the three-mode model. U represents the small-scale driving flow of wave number K (full arrow), v_q is the large-scale perturbation of wave vector q (dashed arrow), and v_Q is the small-scale perturbation of wave vector $Q = K \pm q$ (doted arrow).

prediction and forms a strong peak at the largest scale of the system. A possible explanation for this intriguing result is that a large-scale instability is present.

In pure hydrodynamic flows, the existence of large-scale instabilities has been known for some time. An asymptotic expansion based on scale separation was used in Refs. [11,12] to demonstrate the existence of a mechanism similar to the MHD α -dynamo called the anisotropic-kinetic-alpha (AKA) instability. The AKA instability is present in a certain class of non-parity-invariant, time-dependent, and anisotropic flows. It appears for arbitrary small values of the Reynolds number and leads to a growth rate σ proportional to the wave number q of the unstable mode: $\sigma \propto q$. However, the necessary conditions for the presence of the AKA instability are stricter than those of the α -dynamo. Thus, most archetypal flows studied in the literature do not satisfy the AKA conditions for instability. This, however, does not imply that the large scales are stable since other mechanisms may be present.

In the absence of an AKA effect higher-order terms in the large-scale expansion may lead to a so-called eddy viscosity effect [13]. This eddy viscosity can be negative and thus produce a large-scale instability [14,15]. The presence of a negative eddy viscosity instability appears only above a critical value of the Reynolds number. It results in a weaker growth rate than the AKA effect, proportional to the square of the wave number of the unstable mode $\sigma \propto q^2$. Furthermore, the calculations of the eddy viscosity coefficient can be much more difficult than those of the AKA α coefficient. This difficulty originates at the order at which the Reynolds number enters the expansion as we explain below.

In the present paper, the Reynolds number is defined as $Re \equiv U_{rms}\ell/\nu$ where U_{rms} is the root mean square value of the velocity and ν is the viscosity. Note that we have chosen to define the Reynolds number based on the energy injection scale ℓ . An alternative choice would be to use the domain length scale L, which would lead to the large-scale Reynolds number that we will denote as $Re^L = UL/\nu = (L/\ell)Re$. For the AKA effect, the large-scale Reynolds number Re^L is large, while the Reynolds number Re, based on the forcing scale ℓ , is small. This allows to explicitly solve for the small-scale behavior and obtain analytic results. This is not possible for the eddy viscosity calculation where there are two regimes to consider. Either the Reynolds number is small and the eddy viscosity provides only a small correction to the regular viscosity, or the Reynolds numbers is large and the inversion of an advection operator is needed. This last case can be obtained analytically only for very simple one-dimensional shear flows [14,15].

To illustrate the basic mechanisms involved in such multiscale interactions, we depict in Fig. 1 a toy model demonstrating the main ideas behind these instabilities. This toy model considers a driving flow, U at wave number $|\mathbf{K}| \sim 1/\ell$, that couples to a small amplitude large-scale flow, v_q at wave number $|\mathbf{q}| \sim 1/\ell$ with $|\mathbf{q}| \ll |\mathbf{K}|$. The advection of v_q by U and vice versa will then generate a secondary flow v_Q at wave vectors $\mathbf{Q} = \mathbf{K} \pm \mathbf{q}$. This small-scale perturbation in turn couples to the driving flow and feeds back the large-scale flow. If this feedback is constructive enough to overcome viscous dissipation, it will amplify the large-scale flow, and this process will lead to an exponential increase of v_q and v_Q . This toy model has most of the ingredients required for the instabilities to occur.

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For the full flow, in order to study independently the large-scale instabilities, they must be isolated from other small-scale competing instabilities that might coexist. This can be achieved using Floquet theory [16] (also referred as Bloch theory in quantum mechanics [17]). Indeed, Floquet theory decomposes the unstable flow to modes of different spacial periodicity that evolve independently. This enables us to study precisely large and small spatial periodicity separately. In addition the formalism of Floquet theory allows the study of arbitrary large-scale separation between the smallest scale of the driving flow and the largest scale of the unstable mode without including the intermediate scales. This minimizes the computational cost and permits us to have a systematic study for a wide range of both scale separation and Reynolds numbers without using any approximations.

In what follows, we use direct numerical simulations (DNSs) in the Floquet framework to study large-scale instabilities for different flows. Our aim is to go beyond the range of validity of the asymptotic results (obtained rigorously only at the Re \ll 1 limit) and measure the values of the α coefficient and eddy viscosity for arbitrary Re when this description is applicable. In addition we extend our investigation to turbulent flows that respect a given periodicity, which in general cannot be treated analytically. This allows us to quantify the effect of small-scale turbulence in the large scales. Finally, we compare the results of the Floquet DNS to those of the full Navier-Stokes DNS to test nonlinear effects on the instabilities.

This paper is structured as follows. Section II describes in detail the setup of the problem we are studying and the methods used. Section III gives the results for the linear instability of four different flows, as well us the results from the nonlinear evolution of the instability. Our conclusions are drawn in Sec. IV.

II. METHODS

A. Navier-Stokes

Our starting point is the incompressible Navier-Stokes equation in the periodic $[0,2\pi L]^3$ cube:

$$\partial_t V = V \times \nabla \times V - \nabla P + \nu \Delta V + F, \tag{1}$$

with $\nabla \cdot V = 0$ and where V, F, P, and ν denote the velocity field, the forcing field, the generalized pressure field, and the viscosity coefficient, respectively. The geometry imposes that all fields be $2\pi L$ -periodic. We further assume that the forcing has a shorter spatial period $2\pi \ell$ with L/ℓ an arbitrary large integer. We denote the wave vector of this periodic forcing as \mathbf{K} , with $K = |\mathbf{K}| = 1/\ell$ for the flows examined. If the initial conditions of \mathbf{V} satisfy the same periodicity as F, then this periodicity will be preserved by the solutions of the Navier-Stokes and corresponds to the preservation of the discrete symmetries $x \to x + 2\pi \ell$, $y \to y + 2\pi \ell$, and $z \to z + 2\pi \ell$. However, these solutions can be unstable to arbitrary small perturbations that break this symmetry and grow exponentially. To investigate the stability of the periodic solutions, we decompose the velocity and pressure field in a driving flow and a perturbation component:

$$V = U + v, \quad P = P_U + P_v, \tag{2}$$

where U denotes the driving flow that has the same periodicity as the forcing $2\pi \ell$ and v is the velocity perturbation. The linear stability analysis amounts to determining the evolution of small-amplitude perturbations so that only the first order terms in v are kept. The evolution equation of the driving flow is thus

$$\partial_t U = U \times \nabla \times U - \nabla P_U + \nu \Delta U + F.$$
(3)

The remaining terms give the linearized Navier-Stokes equation for the perturbation:

$$\partial_t \boldsymbol{v} = \boldsymbol{U} \times \boldsymbol{\nabla} \times \boldsymbol{v} + \boldsymbol{v} \times \boldsymbol{\nabla} \times \boldsymbol{U} - \boldsymbol{\nabla} p_{\boldsymbol{v}} + \boldsymbol{v} \Delta \boldsymbol{v}, \tag{4}$$

The two pressure terms enforce the incompressibility conditions $\nabla \cdot U = 0$ and $\nabla \cdot v = 0$. The U flow is not necessarily a laminar flow (but respects $2\pi \ell$ periodicity). In general, the linear perturbation

v does not only consist of modes that break the periodicity of the forcing. Linear unstable modes respecting the periodicity may also exist: they correspond to small-scale instabilities. We show how these modes can be distinguished from periodicity-breaking large-scale modes in the following section devoted to Floquet analysis.

B. Floquet analysis

Studying large-scale flow perturbations with a code that solves the full Navier-Stokes equation requires considerable computational power as resolution of all scales from domain size L to the smallest viscous scales $\ell_{\nu} \ll \ell$ must be achieved. This is particularly difficult in our case where scale separation $\ell \ll L$ is required. In order to overcome this limitation, we adopt the Floquet framework [16]. In Floquet theory, the velocity perturbation can be decomposed into modes that are expressed as the product of a complex harmonic wave, $e^{iq \cdot \mathbf{r}}$, multiplied by a periodic vector field $\tilde{v}(\mathbf{r},t)$ with the same periodicity $2\pi\ell$ as that of the driving flow:

$$\boldsymbol{v}(\boldsymbol{r},t) = \tilde{\boldsymbol{v}}(\boldsymbol{r},t)e^{i\boldsymbol{q}\cdot\boldsymbol{r}} + \text{c.c.},\tag{5}$$

and similar for the pressure,

$$p_{\boldsymbol{v}}(\boldsymbol{r},t) = \tilde{p}(\boldsymbol{r},t)e^{i\boldsymbol{q}\cdot\boldsymbol{r}} + \text{c.c.},\tag{6}$$

where c.c. denotes the complex conjugate of the previous term.

Perturbations whose values of \mathbf{q} are such that at least one component is not an integer multiple of $1/\ell$ break the periodicity of the driving flow. The perturbation field \mathbf{v} then involves all Fourier wave vectors of the type $\mathbf{Q} = \mathbf{q} + \mathbf{k}$, where \mathbf{k} is a wave vector corresponding to the $2\pi\ell$ -periodic space dependence of $\tilde{\mathbf{v}}$. We restrict the study to values of $q = |\mathbf{q}|$ satisfying $0 < q \leq K$. For finite domain sizes \mathbf{q} is a discrete vector with $q \ge 1/L$, while for infinite domain sizes \mathbf{q} can take any arbitrarily small value. In the limit $q/K \ll 1$ the perturbation involves scales much larger than ℓ . Therefore, scale separation is achieved without solving intermediate scales as would be required if the full Navier-Stokes equations were used. Furthermore, this framework has the advantage of isolating perturbations that break the forcing periodicity ($q\ell \notin \mathbb{Z}^3$), from other small-scale unstable modes with the same periodicity ($q\ell \in \mathbb{Z}^3$) that might also exist in the system.

A drawback of the Floquet decomposition is that some operators have somewhat more complicated expressions than in the simple periodic case. For instance, taking a derivative requires to take into account the variations of both the harmonic and the amplitude. Separating the amplitude in its real and imaginary parts $\tilde{v}(\mathbf{r},t) = \tilde{v}^r + \iota \tilde{v}^i$, we obtain

$$\partial_x \boldsymbol{v} = [\partial_x \tilde{\boldsymbol{v}}^r - q_x \tilde{\boldsymbol{v}}^l + \iota(q_x \tilde{\boldsymbol{v}}^r + \partial_x \tilde{\boldsymbol{v}}^l)] e^{\iota \boldsymbol{q} \cdot \boldsymbol{r}} + \text{c.c.}, \tag{7}$$

where ∂_x denotes the *x* derivative and q_x denotes the *x* component of the *q* wave vector.

Using Eqs. (4) and (7), the linearized Navier-Stokes equation can be written as a set of 3 + 1 complex scalar equations:

$$\partial_t \tilde{\boldsymbol{v}} = (\nabla \times \boldsymbol{U}) \times \tilde{\boldsymbol{v}} + (\iota \boldsymbol{q} \times \tilde{\boldsymbol{v}} + \nabla \times \tilde{\boldsymbol{v}}) \times \boldsymbol{U} - (\iota \boldsymbol{q} + \nabla)\tilde{\boldsymbol{p}} + \nu(-\boldsymbol{q}^2 + \Delta)\tilde{\boldsymbol{v}}, \tag{8}$$

with

$$\iota \boldsymbol{q} \cdot \tilde{\boldsymbol{v}} + \boldsymbol{\nabla} \cdot \tilde{\boldsymbol{v}} = 0. \tag{9}$$

We use standard pseudospectral methods to solve this system of equations in the $2\pi \ell$ -periodic cube. The complex velocity field \tilde{v} is decomposed in Fourier space where derivatives are reduced to a multiplication by ιk , where k is the Fourier wave vector. Multiplicative term are computed in real space. These methods have been implemented in the Floquet Linear Analysis for Spectral Hydrodynamics (FLASHy) code, and details are given in the Appendix.

In order to find the growth rate of the most unstable mode, we integrate Eqs. (8) and (9) for a time long enough for a clear exponential behavior to be observed. The growth rate of this most unstable mode can then be measured by linear fitting. Note that this process leads only to the measurement of the fastest growing mode.

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C. Three-mode model

Although the Floquet framework is very convenient to solve equations numerically, it does not easily yield analytic results. Rigorous results must be based on asymptotic expansions and can be derived only in the limit of large Reynolds number [18] or small Reynolds number [14] or for simple shear layers [15]. To obtain a basic understanding of the processes involved, we will use the idea represented in the toy model of Fig. 1. This model also has the major advantage of using a formalism that can easily be related to the physical aspect of the problem.

In our derivation, we only consider the evolution of the two most intense modes of the perturbation and of the driving flow. The velocity perturbation is thus decomposed as a series of velocity fields of different modes:

$$\boldsymbol{v}(\boldsymbol{r},t) = \boldsymbol{v}_{\boldsymbol{q}}(\boldsymbol{r},t) + \boldsymbol{v}_{\boldsymbol{Q}}(\boldsymbol{r},t) + \boldsymbol{v}_{\boldsymbol{>}}(\boldsymbol{r},t), \tag{10}$$

$$\boldsymbol{v}_{\boldsymbol{q}}(\boldsymbol{r},t) = \tilde{\boldsymbol{v}}(\boldsymbol{q},t)e^{i\boldsymbol{q}\boldsymbol{r}} + \text{c.c.},\tag{11}$$

$$\boldsymbol{v}_{\boldsymbol{\varrho}}(\boldsymbol{r},t) = \sum_{||\boldsymbol{k}||=1} \tilde{\boldsymbol{v}}(\boldsymbol{q},\boldsymbol{k},t) e^{\iota(\boldsymbol{q}\cdot\boldsymbol{r}+\boldsymbol{k}\cdot\boldsymbol{r})} + \text{c.c.}, \qquad (12)$$

$$\boldsymbol{v}_{>}(\boldsymbol{r},t) = \sum_{||\boldsymbol{k}||>1} \tilde{\boldsymbol{v}}(\boldsymbol{q},\boldsymbol{k},t) e^{i(\boldsymbol{q}\cdot\boldsymbol{r}+\boldsymbol{k}\cdot\boldsymbol{r})} + \text{c.c.},$$
(13)

where q denotes the wave vector of the large-scale modes and Q denotes the modes directly coupled to q via the driving flow, since K = 1. At wave vector q, the linearized Navier-Stokes equation can be rewritten as

$$\partial_t \boldsymbol{v}_{\boldsymbol{q}} = \boldsymbol{U} \times \boldsymbol{\nabla} \times \boldsymbol{v}_{\boldsymbol{Q}} + \boldsymbol{v}_{\boldsymbol{Q}} \times \boldsymbol{\nabla} \times \boldsymbol{U} - \boldsymbol{\nabla} p_{\boldsymbol{q}} + \boldsymbol{v} \Delta \boldsymbol{v}_{\boldsymbol{q}}. \tag{14}$$

Assuming that the coupling with the truncated velocity, $v_>$, is negligible with respect to the coupling with the large-scale velocity, v_q , the linearized equation at Q reads

$$\partial_t \boldsymbol{v}_{\boldsymbol{Q}} = \boldsymbol{U} \times \boldsymbol{\nabla} \times \boldsymbol{v}_{\boldsymbol{q}} + \boldsymbol{v}_{\boldsymbol{q}} \times \boldsymbol{\nabla} \times \boldsymbol{U} - \boldsymbol{\nabla} p_{\boldsymbol{Q}} + \boldsymbol{v} \Delta \boldsymbol{v}_{\boldsymbol{Q}}, \tag{15}$$

where p_q and p_Q denote the pressure enforcing the incompressible conditions: $\nabla \cdot \boldsymbol{v}_q = 0$ and $\nabla \cdot \boldsymbol{v}_Q = 0$, respectively.

As of now, the derivation is restricted to stationary positive helical driving flows, satisfying $U_{\mathcal{H}}(\mathbf{r}) = K^{-1} \nabla \times U_{\mathcal{H}}(\mathbf{r})$. The problem can then be solved by making use of the vorticity fields:

$$\boldsymbol{\omega}_{\boldsymbol{q}} = \boldsymbol{\nabla} \times \boldsymbol{v}_{\boldsymbol{q}} \quad \text{and} \quad \boldsymbol{\omega}_{\boldsymbol{Q}} = \boldsymbol{\nabla} \times \boldsymbol{v}_{\boldsymbol{Q}}, \tag{16}$$

and the adiabatic approximation, $\partial_t \boldsymbol{v}_{\boldsymbol{Q}} \ll \nu \Delta \boldsymbol{v}_{\boldsymbol{Q}}$. The system of equations of the three-mode model is thus

$$\nu \Delta \boldsymbol{\omega}_{\boldsymbol{Q}} = -\nabla \times [\boldsymbol{U}_{\mathcal{H}} \times (\boldsymbol{\omega}_{\boldsymbol{q}} - \boldsymbol{K} \boldsymbol{v}_{\boldsymbol{q}})], \tag{17}$$

$$\partial_t \boldsymbol{\omega}_q = \boldsymbol{\nabla} \times [\boldsymbol{U}_{\mathcal{H}} \times (\boldsymbol{\omega}_Q - \boldsymbol{K} \boldsymbol{v}_Q)] + \boldsymbol{\nu} \Delta \boldsymbol{\omega}_q.$$
(18)

The greatest eigenvalue of the system, σ , gives the growth rate of the perturbation. The growth rate can be derived analytically for an *ABC* large-scale flow:

$$U_x^{ABC} = C\sin(Kz) + B\cos(Ky), \tag{19}$$

$$U_{y}^{ABC} = A\sin(Kx) + C\cos(Kz), \qquad (20)$$

$$U_z^{ABC} = B\sin(Ky) + A\cos(Kx).$$
(21)

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FIG. 2. Growth rate of the perturbation plotted as a function of the Floquet wave number in log-log scale for a Fr87 flow [Eq. (24)]. The different markers represent data for different Reynolds numbers. The solid lines placed above the different sets of markers represent the theoretical prediction.

For A = 1: B = 1: $C = \lambda$ flows ($\lambda - ABC$), one finds

$$\sigma = \beta q^2 - \nu q^2 \quad \text{with} \quad \beta = b \text{Re}^2 \nu, \tag{22}$$

$$b = \frac{1 - \lambda^2}{4 + 2\lambda^2}$$
 and $\operatorname{Re} = \frac{U}{K\nu}$, (23)

where Re denotes the small-scale Reynolds number defined using the driving flow. The fastest growing mode is found to be fully helical.

This simple model indicates that some driving flows, not satisfying the hypotheses of the AKA effect, described in Ref. [11], can generate a negative eddy viscosity instability satisfying $\sigma \propto q^2$. The largest growth rate is obtained for $\lambda = 0$ while no q^2 instability is predicted for $\lambda = 1$. For $\lambda \neq 1$ the flow becomes unstable when the β term can overcome the viscosity $\beta > \nu$. This happens when Re is above a critical value: Re^c = $b^{-1/2}$.

III. RESULTS

A. AKA

We begin by examining a flow that satisfies the conditions for an AKA instability. Such a flow was proposed in Ref. [11] (hereafter Fr87) and is given by

$$U_{x}^{\text{Fr87}} = U_{0} \cos(Ky + \nu K^{2}t),$$

$$U_{y}^{\text{Fr87}} = U_{0} \sin(Kx - \nu K^{2}t),$$

$$U_{z}^{\text{Fr87}} = U_{x}^{\text{Fr87}} + U_{y}^{\text{Fr87}}.$$
(24)

The growth rate of large-scale unstable modes can be calculated in the small Reynolds number limit and is given by

$$\sigma = \alpha q - \nu q^2, \tag{25}$$

with $\alpha = aU_0$ and $a = \frac{1}{2}$. The fastest growing mode has negative helicity and q along the z direction.

Setting q along the z direction, we integrated Eq. (9) numerically and measured the growth rate σ . Figure 2 displays the growth rate of the most unstable mode as a function of the wave number amplitude q = |q| for three different values of Re measured by the Floquet code and compared to



FIG. 3. The observable related to the α -coefficient [$\langle \sigma/q \rangle / U_0$ using Eq. (25)] plotted as a function of the Reynolds number in log-log scale for an instability generated by a Fr87 flow. The solid line represents the prediction, and the crosses the numeric results collected with the FLASHy code. In the inset, evolution of the growth rate of the perturbation represented as a function of the Floquet wave number. The results are plotted in log-log scale at various Reynolds numbers for a Fr87 flow [Eq. (24)]. The solid line represents the theoretical scaling law.

the theoretical prediction. The agreement is good for small values of q and for small values of Re where the asymptotic limit is valid. For q small enough, the flow is unstable and satisfies $\sigma \propto q$. The inset of Fig. 3 shows in log-log scale the growth rate of the perturbation as a function of q for different Reynolds numbers. The solid line in the graph indicates the $\sigma \propto q$ scaling, which is satisfied for all Re. In Fig. 3 we compare the theoretical and numerically calculated prefactor a of the α coefficient. This coefficient increases linearly with Re and is seen to be in good agreement with the theoretical prediction up to Re $\simeq 10$. For larger values of Re, a deviates from the linear prediction and saturates.

A positive growth rate for a small q mode does not guarantee the dominance of large scales. We should also consider what fraction of the perturbation energy is concentrated in the large scales. Figure 4 shows the energy spectra for different Reynolds numbers. The energy spectrum for the complex Floquet field \tilde{v} is defined as $E(k) = \sum_{k-\frac{1}{2} \le |\mathbf{k}| \le k+\frac{1}{2}} |\tilde{v}|^2$ with E(k = 0) the energy at large scales 1/q. While at small Reynolds numbers, the smallest wave number k = 0 dominates, as the Reynolds number increases, more energy is concentrated in the wave number of the driving flow k = 1.

To quantify this behavior, we plot in the inset of Fig. 5 the fraction of the energy in the zero mode $E_0 = E(0)$ divided by the total energy of the perturbation $E_{\text{tot}} = \sum_{k=0}^{\infty} E(k)$, as a function of the wave number q for different values of Re. In the small q limit, this ratio reaches an asymptote that depends on the Reynolds number. This asymptotic value is shown as a function of the Re in Fig. 5. The small-scale energy ($E_{\text{tot}} - E_0$) is then shown to follow a power law $1 - \frac{E_0}{E_{\text{tot}}} \propto \text{Re}^2$ for small values of Re. Therefore, for the AKA instability, at small Re, the energy is concentrated in the large scales, whereas, at large Re, the most unstable mode has a small projection in the large scales.

B. Roberts flow: $\lambda = 0$

We now investigate non-AKA-unstable flows. We consider the family of the ABC flow, for which we expect large-scale instabilities of the form given in Eq. (23). The three-mode model predicts that



FIG. 4. The energy spectrum of the Floquet perturbation of wave vector $\mathbf{q} = (0; 0; 0.025)$ represented as a function of the Fourier wave number in semilog scale. The Floquet perturbation was generated by a Fr87 flow [Eq. (24)]. Markers of different shapes represent data with different Reynolds numbers.

from the family of *ABC* flows the most unstable is the A = 1: B = 1: C = 0 flow that is commonly referred to as the Roberts flow in the literature [19]. The model predicts a positive growth rate when Re > 2. Figure 6 shows the growth rate σ as a function of q for various Reynolds numbers calculated using the Floquet code. For small values of the Reynolds number all modes q have negative growth rate. Above a critical value Re^c \simeq 2 unstable modes appear at small values of q in agreement with the model predictions.

To investigate the behavior of the instability for small values of q we plot in the inset of Fig. 7 the absolute value of the growth rate as a function of q, in a logarithmic scale, for Reynolds number ranging from 0.312 to 160. Dashed lines indicate positive growth rates, while dotted lines indicate negative growth rates. The solid black line indicates the $\sigma \propto q^2$ scaling followed by all curves.



FIG. 5. Large-scale energy ratio represented as a function of the Reynolds number in log-log scale for a Fr87 flow [Eq. (24)]. The solid line shows the theoretical scaling. In the inset, evolution of the large-scale energy ratio of the perturbation represented as a function of the Floquet wave number. The results are plotted in log-log scale at for different Reynolds numbers for a Fr87 flow.



FIG. 6. Growth rate plotted as a function of the Floquet wave number in log-log scale for a Robert flow. The different markers represent data with different Reynolds numbers.

Therefore, the scaling predicted by the model [Eqs. (22) and (23)] is verified. We will refer to the instabilities that follow this scaling $\sigma \propto q^2$ as negative eddy viscosity instabilities. To further test the model predictions we measure the proportionality coefficient for the q^2 power law obtained from the Floquet code. Figure 7 compares the *b* coefficient predicted by the three-mode model with the



FIG. 7. The observable related to the β -coefficient [$\langle \sigma/q^2 \rangle / \nu + 1$ using Eq. (22)] of the Floquet perturbation generated by a Roberts flow is plotted as a function of the Reynolds number in semilog scale. In the inset, evolution of the growth rate of the perturbation of a Roberts flow represented as a function of the Floquet wave number. The data are presented in log-log scale to highlight the power law. The different markers on the graph represent different Reynolds numbers. The full markers with dashed lines represent the value of positive growth rates, and the empty markers with dots represent the absolute value of negative growth rates. The solid line represents the theoretical predication.



FIG. 8. The large-scale energy ratio represent as a function of the Reynolds number for the most unstable Floquet mode of the Roberts flow. In inset, evolution of the large-scale energy ratio of the perturbation as a function of the Floquet wave number plotted in log-log scale at different Re for a Roberts flow.

results of the Floquet code. The figure shows $(\langle \sigma/q^2 \rangle + \nu)/\nu$ measured from the data for different values of Re, while the Re²/4 prediction of the model is shown by a solid black line. The two calculations agree on nearly two orders of magnitude. Positive growth rate for the large-scale modes implies $\langle \sigma/q^2 \rangle/\nu + 1 > 1$. The critical value of the Reynolds number, for which the instability begins, can be obtained graphically at the intersection of the numerically obtained curve with the $\langle \sigma/q^2 \rangle/\nu + 1 = 1$ line plotted with a dash-dot green line. The predictions of the model Re^c = 2 and the numerically values obtained are in excellent agreement.

Similarly to the AKA flow, the fraction of energy concentrated in the large scales (k = 1) becomes independent of q in the small q limit. This is demonstrated in the inset of Fig. 8 where the ratio of E_0/E_{tot} is plotted as a function of q. In Fig. 8 we show the asymptotic value of this ratio as a function of the Reynolds number. As in the case of the AKA instability, the projection to the large scales depends on the Reynolds number, and at large Re, it follows the power law $\frac{E_0}{E_{\text{tot}}} \propto \text{Re}^{-2}$.

C. Equilateral *ABC* flow: $\lambda = 1$

For the A = 1: B = 1: C = 1 flow, the three-mode model predicts that the *b* coefficient is zero. Therefore, the model does not predict a negative eddy viscosity instability with $\sigma \propto q^2$. Figure 9 shows the growth rate as a function of the wave number *q* calculated using the Floquet code for different values of the Reynolds number. Clearly the small *q* modes still become unstable, but the dependence on Re appears different from the previously examined cases. We thus examine separately the small Re and large Re behaviors.

1. Small values of Re

First, we examine the instability for small values of $\text{Re} \leq 10$ for which the growth rate σ tends to zero as $q \rightarrow 0$. The inset of Fig. 10 shows the growth rate of the instability for the equilateral *ABC* flow as a function of the wave number q in logarithmic scale for different values of Re ranging from 0.312 to 10. In this range, the growth rate behaves much like the Roberts flow and contradicts the three-mode model. The numerically calculated growth rates show a clear negative eddy viscosity scaling $\sigma \propto q^2$. The growth rate becomes positive above a critical value of Re. In Fig. 10 the measured value of $\langle \sigma/q^2 \rangle / \nu + 1$ is represented as a function of the Reynolds number. In the inset, the plotted lin-log of $\frac{\langle \sigma/q^2 \rangle + \nu}{\text{Re}^2 \nu}$ provides a measurement of the *b* coefficient. This expression



FIG. 9. Growth rate evolution of the perturbation represented as a function of the Floquet wave number for the equilateral *ABC* flow. The different markers represent the evolution of the growth rate of data with different Reynolds numbers.

becomes larger than one (signifying the instability boundary that is marked by a dash-dot line) for Re ≥ 3 . This value Re^c $\simeq 3$ is slightly higher than the critical Reynolds number of the Roberts flow Re^c = 2. At very small Reynolds number, the value of $b = \frac{\langle \sigma/q^2 \rangle + \nu}{Re^2 \nu}$ approaches zero very quickly, which indicates that the model prediction is recovered at Re $\rightarrow 0$.

To investigate further the discrepancy of the Floquet results with the three-mode model. Figure 11 shows the *b* coefficient (measured as $b = \frac{\langle \sigma/q^2 \rangle + \nu}{\text{Re}^2 \nu}$) for different λ parameter from 0 (Roberts flow) to 1 (equilateral *ABC* flow). All the DNS are carried out at Re = 10. The results indicate that the three-mode model and the results from the Floquet code agree for $\lambda \leq 0.5$ but deviate as λ becomes larger. To identify where this discrepancy between the model and the DNS occurs, we modified the FLASHy code in order to test the assumptions of the model. This is achieved by enforcing the



FIG. 10. The observable related to the β -coefficient $[\langle \sigma/q^2 \rangle / \nu + 1]$ using Eq. (22)] of the Floquet perturbation generated by a equilateral *ABC* flow, represented as a function of the Reynolds number in log-log scale. In the inset, evolution of growth rate of the perturbation of a equilateral *ABC* flow represented as a function of the Floquet wave number in log-log scale to highlight the power law. The different markers on the graph represent different Reynolds numbers. The full markers with dashed lines represent the value of positive growth rates, and the empty markers with dots represent the absolute value of negative growth rates.



FIG. 11. The measured values of the *b* coefficient represented as a function of the λ -parameter of the flow (*ABC* flow with $A = 1 : B = 1 : C = \lambda$) for Re = 10. The dashed curves with crosses represents the numeric data collected with the FLASHy code. The full line curve with circle represents the prediction given by the three-mode model.

adiabatic approximation in the Floquet code and by controlling the number of modes that play a dynamical role. The latter is performed by using a Fourier truncation of the Floquet perturbation at a value k_{cut} so that only modes with $k < k_{\text{cut}}$ are present. Figure 12 shows the dependence of the *b* coefficient on the truncation mode, k_{cut} . For $k_{\text{cut}} \ge 3$, the growth rate reaches the asymptotic value that is also observed in the inset of Fig. 10 for Re = 10 obtained from the "untampered" FLASHy code. This confirms the assumption that modes in the smallest scales have little impact on the evolution of the large-scale perturbation. However, the *b* coefficient strongly varies for $k_{\text{cut}} \le 3$. The model predictions are recovered only when $k_{\text{cut}} = 1$, which amounts to keeping only the modes used in the model. Therefore, the hypothesis of the model to restrict the interaction of the perturbation to its first two Fourier modes does not seem to hold for the equilateral *ABC* flow at moderate Reynolds



FIG. 12. The values of the *b* coefficient computed by the FLASHy code are represented as a function of the truncation imposed in the code. The perturbation was generated by equilateral *ABC* flow at Re = 10.



FIG. 13. Evolution of growth rate of the perturbation generated by an equilateral *ABC* flow at large values of Re represented as a function of the Floquet wave number. The different markers represent data with different Reynolds number.

number, $1 \leq \text{Re} \leq 10$. The adiabatic hypothesis does not appear to affect the results. Therefore, the discrepancy between the three-mode model and the numeric results is due to the coupling of the truncated velocity $v_>$ that was neglected in the model.

2. Large values of Re

We now turn our focus to large values of the Reynolds number that display a finite growth rate σ at $q \rightarrow 0$; see Fig. 9. Figure 13 shows the growth rate σ in a lin-log scale for four different values of the Reynolds number. Unlike the small values of Re examined before here it is clearly demonstrated that above a critical value of Re the growth rate σ reaches an asymptotic value independent of q. At first, this finite growth rate seems to violate the momentum conservation. Indeed, momentum conservation enforces modes with q = 0, corresponding to uniform flows, not to grow.

The resolution of this conundrum can be obtained by looking at the projection of the unstable modes to the large scales. In Fig. 14 we plot the ratio E_0/E_{tot} as a function of q for the same values of Re as used in Fig. 13. Unlike the small Re cases examined previously, for large Re, this energy ratio decays to zero at small values of q and appears to follow the power law $E_0/E_{tot} \propto q^4$. Therefore, at q = 0, the energy at large scales E_0 is zero and the momentum conservation is not violated in the q = 0 limit.

3. Small- and large-scale instabilities

The results of the previous sections indicate that there are two distinct behaviors: the first one for which $\lim_{q\to 0} \sigma = 0$ and $\lim_{q\to 0} E_0/E_{tot} > 0$ when Re is small, and the second one for which $\lim_{q\to 0} \sigma > 0$ and $\lim_{q\to 0} E_0/E_{tot} = 0$ when Re is large. We argue that there is a second critical Reynolds number Re_S^c such that flows for which $\operatorname{Re}^c < \operatorname{Re} < \operatorname{Re}_S^c$ show the first behavior, while flows with $\operatorname{Re}_S^c < \operatorname{Re}$ show the second behavior. This second critical value is related to the onset of small-scale instabilities.

To demonstrate this claim we are going to use a simple model. We consider the evolution of two modes, one at large scales v_q and one at small scales v_q . These modes are coupled together by an external field U. In the absence of this coupling, the large-scale mode v_q decays while the evolution of the small-scale mode v_q depends on the value of the Reynolds number. The simplest model satisfying these constraints, dimensionally correct and leading to an AKA type $\sigma \propto q$ instability or



FIG. 14. Evolution of the large-scale energy ratio of the perturbation generated by an equilateral *ABC* flow at large values of Re represented as a function of the Floquet wave number. The different markers represent data with different Reynolds number.

a negative eddy viscosity instability $\sigma \propto q^2$, is

$$\frac{d}{dt}v_q = -\nu q^2 v_q + U q^n Q^{1-n} v_\varrho, \qquad (26)$$

$$\frac{d}{dt}v_Q = UQv_q + \sigma_Q v_Q.$$
⁽²⁷⁾

The index *n* takes the values n = 1 if an AKA instability is considered and n = 2 if an instability of negative eddy viscosity is considered. Note that for q = 0 the growth of v_q is zero, as required by momentum conservation. $\sigma_q = sUQ - vQ^2$ gives the small-scale instability growth rate that is positive if $\text{Re} = U/(vQ) > 1/s = \text{Re}_s^c$.

The simplicity of the model allows for an analytic calculation of the growth rate and the eigenmodes. Despite its simplicity, it can reproduce most of the results obtained here in the $q \ll Q$ limit. The general expression for the growth rate is given by $\sigma = \frac{1}{2}[(\sigma_{\varrho} - \nu q^2 \pm \sqrt{(\sigma_{\varrho} + \nu q^2)^2 + 4Q^{2-n}q^n U^2}]$ and eigenmode satisfies $v_q/v_{\varrho} = Uq^n Q^{1-n}/(\sigma + \nu q^2)$.

First, we focus on large values of v such that $\sigma_{\varrho} = -vQ^2 < 0$. For n = 1, the growth rate σ and the energy ratio $E_0/E_{\text{tot}} = v_q^2/(v_q^2 + v_{\varrho}^2)$ are given to the first order in q

$$\sigma \simeq \frac{U^2 q}{\nu Q}$$
 and $\frac{E_0}{E_{\text{tot}}} \simeq \frac{1}{1 + \text{Re}^2}$. (28)

In the same limit for n = 2 we obtain

$$\sigma \simeq \nu (\operatorname{Re}^2 - 1)q^2 \quad \text{and} \quad \frac{E_0}{E_{\text{tot}}} \simeq \frac{1}{1 + \operatorname{Re}^2}.$$
 (29)

The critical Reynolds number for the large-scale instability is given by $\text{Re}^c = 1$. Both of these results in Eqs. (28) and (29) are in agreement with the results demonstrated in Figs. 3, 5, 7, and 8.

The behavior changes when a small-scale instability exists $\sigma_Q > 0$. This occurs when $UQ > s\nu Q^2$ at the critical Reynolds number: $\operatorname{Re}_S^c = 1/s$. For large $\operatorname{Re} \gg \operatorname{Re}_S^c$ we thus expect $\sigma_Q \simeq sUQ > 0$. In this case for n = 1 to first order in q, we have

$$\sigma \simeq \sigma_{\varrho} \quad \text{and} \quad \frac{E_0}{E_{\text{tot}}} \simeq \frac{q^2}{s^2 Q^2},$$
(30)

while for n = 2, we obtain

$$\sigma \simeq \sigma_{\varrho} \quad \text{and} \quad \frac{E_0}{E_{\text{tot}}} \simeq \frac{q^4}{s^2 Q^4}.$$
 (31)

The model is thus in agreement also with the scalings observed in Figs. 13 and 14. The transition from one behavior to the other occurs at the onset of small-scale instability Re_S^c . It is thus worth pointing out that the results of the FLASHy codes showed that the transition from $\lim_{q\to 0} \sigma = 0$ modes to $\lim_{q\to 0} \sigma > 0$ occurs at the value of Re for which small-scale instability of the *ABC* flow starts at $\text{Re}_S^c \simeq 13$; see Refs. [20,21]. This further verifies that the transition observed is due to the development of small-scale instabilities.

We also note here that both the Roberts flow and the Fr87 flow given in Eq. (24) are invariant in translations along the z direction. This implies that each q_z mode evolves independently with out coupling to other k_z modes. The onset of small-scale instabilities Re_S^c for q = 0 in this case then corresponds to the onset of two-dimensional instabilities. Two-dimensional flows, however, forced at the largest scale of the system are known to be stable at all Reynolds numbers [22]. This result originates from the fact that two-dimensional flows conserve both energy and enstrophy, and small scales cannot be excited without exciting large scales at the same time. This is the reason why no Re_S^c were observed in these flows.

D. Turbulent equilateral ABC flows

As discussed in the introduction the driving flow does not need to be laminar to use Floquet theory. It is only required to obey the $2\pi \ell$ -periodicity. It is worth thus considering large-scale instabilities in a turbulent *ABC* flow that satisfies the forcing periodicity. This amounts to the turbulent flow forced by an *ABC* forcing in a periodic cube of the size of the forcing period $2\pi \ell$. Due to the stationarity of the laminar *ABC* flow, it can be excluded as a possible candidate for an AKA instability. However, this is not true of a turbulent *ABC* flow since it evolves in time. We cannot thus *a priori* infer that a turbulent *ABC* flow results in an AKA instability or not.

To test this possibility, we consider the linear evolution of the large-scale perturbations v driven by an equilateral *ABC* flow at Re = 50, which is beyond the onset of the small-scale instability Re^c_S \simeq 13. The turbulent equilateral *ABC* flow **U** is obtained solving the Navier-Stokes equations (3) in the domain $(2\pi \ell)^3$ driven by the forcing function $\mathbf{F}^{ABC} = \mathbf{U}^{ABC}$. The code is executed until the flow reaches saturation. The evolution of the large scale perturbations is then examined solving Eq. (9) with the FLASHy code coupled to the Navier-Stokes equations (3).

The kinetic energy E_U of the turbulent equilateral *ABC* flow **U** is shown in Fig. 15. The energy E_U strongly fluctuates around a mean value. The evolution of the energy E_{tot} of the perturbations **v** for different values of q is shown in the inset of Fig. 16. E_{tot} shows an exponential increase, from which the growth rate can be measured. The growth rate σ as a function of the wave number q is shown in Fig. 16, and the ratio E_0/E_{tot} is shown in Fig. 17. The growth rate of the large-scale instabilities appears to reach an finite value in the limit $q \rightarrow 0$ just like laminar *ABC* flows above the small-scale critical Reynolds Re_S^c . However, the ratio E_0/E_{tot} does not scale like q^4 as laminar equilateral *ABC* flows but like q^2 . This indicates that the turbulent equilateral *ABC* flow has a stronger effect on the large scales than its laminar version. This can have possible implications for the saturated stage of the instability that we examine next.



FIG. 15. Temporal evolution of the energy of the turbulent equilateral ABC driving flow at Re = 122.

E. Nonlinear calculations and bifurcation diagram

We further pursue our investigation of large-scale instabilities by examining the nonlinear behavior of the flow close to the instability onset. We restrict ourselves to the case of the equilateral *ABC* flow whose nonlinear behavior has been extensively studied in the absence, however, of scale separation [23]. The linear stability of the *ABC* flow in the minimum domain size has been studied in Ref. [20] and more recently in Ref. [24]. These studies have shown that the *ABC* flow destabilizes at $\text{Re}_S^c \simeq 13$.

To investigate the nonlinear behavior of the flow in the presence of scale separation, we perform a series of DNSs of the forced Navier-Stokes equation [Eq. (1)] in triple periodic cubic boxes of size $2\pi L$ using the GHOST code [25,26]. The forcing maintaining the flow is $\mathbf{F}^{ABC} = \frac{\sqrt{2}}{\sqrt{3}} \nu |\mathbf{K}|^2 \mathbf{U}^{ABC}$ so that the laminar solution of the flow is the *ABC* flow [23] normalized to have unit energy. Four



FIG. 16. The growth rate of the perturbation generated by the turbulent equilateral ABC driving flow is represented as a function of the Floquet wave number. In the inset, the exponential growth of the energy of the large-scale perturbations represented as a function of time for various q.



FIG. 17. The large-scale energy ratio is represented as a function of the Floquet wave number for a perturbation forced by a turbulent equilateral ABC flow. The dashed line with the crosses represents the numeric results and the solid line the scaling law.

different boxes sizes are considered: KL = 1, 5, 10, and 20. For each box size and for each value of Re, the flow is initialized with random initial conditions and evolves until a steady state is reached.

Figure 18 shows the saturation level of the total energy E_V at steady state as a function of Re for the four different values of KL. At low Reynolds number, the laminar solution $\mathbf{V} = \mathbf{U}^{ABC}$ is the only attractor, and so the energy is $E_V = 1$. At the onset of the instability the total energy decreases. A striking difference appears between the KL = 1 case and other three cases. For the KL = 1 case the first instability appears at $\text{Re}_S^c \simeq 13$ in agreement with the previous work [20,24]. By definition, only small-scale instabilities are present in the KL = 1 case (i.e., instabilities that do not break the forcing periodicity). For the other three cases, which allow the presence of modes of larger scale



FIG. 18. Bifurcation: the total energy of the flow is represented as a function of the Reynolds number for different scale separation $K \in \{1; 5; 10; 20\}$. In the inset, zoom of the graph of the total energy near the large-scale bifurcation for Re $\in [2; 5]$.



FIG. 19. The energy spectra of the flow in the large-scale instability bifurcation plotted for different scale separations $K \in \{1; 5; 10; 20\}$.

than the forcing scale, the flow becomes unstable at a much smaller value: $\text{Re}^c \simeq 3$. This value of Re^c is in agreement with the results obtained in Sec. III C for large-scale instability by a negative eddy viscosity mechanism. The energy curves for the forcing modes $KL \ge 5$ all collapse on the same curve. This indicates that not only the growth rate but also the saturation mechanism for these three simulations are similar.

Further insight on the saturation mechanism can be obtained by looking at the energy spectra. Figure 19 shows the energy spectrum of the velocity field at the steady state of the simulations. Two types of spectra are plotted. In Fig. 19, spectra plotted using lines and denoted as k-bin display energy spectrum collected in bins where modes **k** satisfy $n_1 - 1/2 < |\mathbf{k}| L \leq n_1 + 1/2$, with n_1 a positive integer. E(k) then represents the energy in the bin $n_1 = k$. In Fig. 19 spectra plotted using red dots and denoted by k^2 -bin display the energy spectrum collected in bins where modes **k** satisfy $|\mathbf{k}|^2 L^2 = n_2$, with n_2 a positive integer. Since $\mathbf{k}L$ is a vector with integer components m_x, m_y , and m_z , its norm $k^2 L^2 = m_x^2 + m_y^2 + m_z^2$ is also a positive integer. E(k) then represents the energy distribution among modes. In our case, they help separate K modes from $K \pm 1/L$ modes and highlight the three-mode interaction. The $k = K \pm 1/L$ modes as well as the largest scale mode kL = 1 that were used in the three-mode model are shown by blue circles in the spectra. The drawback of k^2 -bin spectra is their memory consumption. They have a number of bins equal to the square of the number of bins of standard k-bin spectra. However, since spectra are not outputted at every time step, this inconvenience is limited.

The plots of the spectra show that the most energetic modes are the modes close to the forcing scale and the largest scale mode kL = 1. This is true even for the largest scale separation examined

KL = 20. We note that the largest scale mode is not the most unstable one as seen in all the cases examined (see Figs. 2, 6, and 9). Despite this fact, it appears that the kL = 1 is the dominant mode that controls saturation. The exact saturation mechanism, however, is beyond the scope of this work.

IV. CONCLUSION

In this work, using the Floquet framework as well as simplified models, we examined in detail the large-scale hydrodynamic instabilities for a variety of flows. The Floquet framework allowed us to distinguish small- from large-scale instabilities in a rigorous manner and study the evolution of the latter independently for a wide parameter range. The results depend on the type of flow under study and the value of the Reynolds number.

More precisely it was shown that for the Fr87 flow [see Eq. (24)] and for small values of Re, the instability growth rate scales like $\sigma \propto q \operatorname{Re}^c$, with most of the energy in the large scales $1 - E_0/E_{\text{tot}} \propto \operatorname{Re}^2$. It is present for any arbitrarily small value of the Reynolds number provided that scale separation is large enough. The linear scaling of the growth rate with q persisted for values of Re beyond the asymptotic regime with the prefactor becoming independent of Re at sufficiently large Re.

Flows without an AKA instability, like the *ABC* and Roberts flow, show a negative eddy viscosity scaling. The instability appears only above a critical value of the Reynolds number Re^c that was found to be $\text{Re}^c \simeq 2$ for the Roberts flow and $\text{Re}^c \simeq 3$ for the equilateral *ABC* flow. The growth rate follows the scaling $\sigma \propto \nu (b\text{Re}^2 - 1)q^2$. The value of *b* can be calculated based on a three-mode model for the Roberts flow and was found to be b = 1/4. The three-mode model however failed to predict the *b* coefficient of the equilateral *ABC* flow because more modes were contributing to the instability.

For the equilateral *ABC* flow the negative eddy viscosity scaling $\sigma \propto q^2$ was shown to stop at a second critical Reynolds number Re_S^c , where the flow becomes unstable to small-scale perturbations. For values of Re larger than Re_S^c the growth rate remains finite and independent of q ($\sigma \propto q^0$) at the $q \rightarrow 0$ limit. On the contrary, the fraction of energy at the largest scale becomes dependent on q decreasing as $E_0/E_{\text{tot}} \propto q^4$ as $q \rightarrow 0$. This behavior is well described by a two-mode model that is explained in Sec. III C 3.

The scaling of the growth rate $\sigma \propto q^0$ was also observed for the turbulent ABC flow that was also examined in this work. However, the projection on the large scales of the unstable mode was stronger than the laminar flow following the scaling $E_0/E_{tot} \propto q^2$, implying that the turbulent flow is more effective at exciting large scales. We note that a turbulent or chaotic flow is by definition small-scale unstable with a growth rate of the unstable modes proportional to the Lyaponov exponent of phase-space trajectories. For this reason, any flow with Re that is large enough for the flow to be turbulent cannot display a $\sigma \propto q$ or $\sigma \propto q^2$ scaling. We further note that the observed scaling cannot be expressed in terms of a turbulent α effect or a turbulent viscosity. This can have important implications on subgrid models commonly used in numerical codes. These models mimic the effect of unresolved turbulent scales on large eddies and typically have only a damping effect. Our work indicates that small scales are also responsible for the excitation of large scales, an effect that needs to be taken in to account.

Finally our study was carried out further to the nonlinear regime where the saturation of the large-scale instabilities was examined for four different box sizes. The presence of scale separation alters the bifurcation diagram, with the large-scale modes playing a dominant role in the saturation mechanism. The saturation amplitude of the energy of the large-scale instability appears to be independent of the scale separation and of larger amplitude than in the absence of scale separation. This indicates that studying small-scale turbulence isolated from any large-scale effects could also be misleading. The persistence of this behavior at larger values of Re remains to be examined.

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APPENDIX: FLASHY

A pseudospectral method is adopted to compute numerically Eqs. (8) and (9). The linear term is computed in Fourier space. All the terms involving the driving flow are computed in physical space made incompressible by solving in periodic space the Poisson problem, using

$$\Psi^{(2)} = -\Delta^{-1} (\nabla \times)^2 \Psi^{(1)}. \tag{A1}$$

The main steps of the algorithm are given below. In this algorithm, \mathcal{F} and \mathcal{F}^{-1} denote direct and inverse fast Fourier transforms. $AUX^{(1)}$ and $AUX^{(2)}$ are two auxiliary vector fields.

Floquet Linear Analysis of Spectral Hydrodynamic FLASHy

Require: $v, T, dt, q, v^{(0)}, U$ 1: $\Omega = \nabla \times U$ 2: n = 03: $V^{(n)} = \mathcal{F}(v^{(n)})$ 4: while t < T do 5: $AUX^{(1)} = U \times \mathcal{F}^{-1}(\iota(k+q) \times V^{(n)}) - \Omega \times \mathcal{F}^{-1}(V^{(n)})$ 6: $AUX^{(2)} = -||k+q||^{-2}(k+q) \times (k+q) \times \mathcal{F}[AUX^{(1)}]$ 7: $V^{(n+1)} = V^{(n)} + dt(AUX^{(2)} - v||k+q||^2 vV^{(n)})$ 8: n = n + 1, t = t + dt9: end while

To carry out the computations with greater precision, a fourth order Runge-Kutta method is used instead of the simple Euler method at line 7 of the algorithm. The Fourier parallel expansions are also truncated at 1/3 to avoid aliasing error. The code is parallelized with MPI and uses many routine from the GHOST code [25,26]. Most of the DNSs are done at a 32^3 and 64^3 resolution. Convergence tests show that this resolution is sufficient for the range of Reynolds number studied.

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